

1 **Bayesian Updating of Earthquake**
2 **Vulnerability Functions with Application to**
3 **Mortality Rates**

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5 Vulnerability functions often rely on data from expert opinion, post-
6 earthquake investigations, or analytical simulations. Combining the
7 information can be particularly challenging. In this paper a Bayesian
8 statistical framework is presented to combining disparate information. The
9 framework is illustrated through application to earthquake mortality data
10 obtained from the 2005 Pakistan earthquake and from PAGER. Three
11 different models are tested including an exponential, a combination of
12 Bernoulli and exponential and Bernoulli and gamma fit to model respectively
13 zero and non-zero mortality rates. A novel Bayesian model for the Bernoulli-
14 exponential and Bernoulli-gamma probability densities is introduced. It is
15 found that the exponential distribution represents the zero casualties very
16 poorly. The Bernoulli-exponential and Bernoulli-gamma models capture the
17 data for both the zero and non-zero mortality rates. It is also shown that the
18 Bernoulli-gamma model fits the 2005 Pakistan data the best and has
19 uncertainties that are smaller than either the ones from the 2005 Pakistan data
20 or the PAGER data.

21

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INTRODUCTION

23 When developing vulnerability or fragility functions, information is often limited and
24 comes in different forms such as expert opinion, data from post-earthquake
25 investigations, or analytical simulations. Combining the information from various sources

26 can be particularly challenging. Singhal and Kiremidjian (1998) first proposed the use of
27 Bayesian statistics to combine heuristic information with numerically simulated data for
28 developing fragility functions for reinforced concrete structures. Several other studies
29 have also deployed Bayesian statistical methods for fragility analysis of structures (e.g.
30 Choe et al. 2007; Der Kiureghian 1999a, b, 2002; Gardoni et al. 2002; Gardoni et al.
31 2003; Huang et al. 2010; Koutsourelakis 2010; Zhong et al. 2008). In this paper a
32 Bayesian statistical framework is presented to enable a systematic approach for
33 combining disparate information for developing casualty rates from collapsed buildings.
34 The focus of the paper is on the development of vulnerability rates that require different
35 probability distributions to model zero and nonzero mortality rates. The Bayesian
36 treatment of the exponential distribution fit to mortality rates is developed as an example
37 of conventional Bayesian updating of probability distributions. The paper presents a
38 novel approach to Bayesian updating of combination of probability distributions for
39 mortality rate analysis, in this case the combination of Bernoulli with exponential and
40 Bernoulli with gamma probability densities. The approach presented in the paper is
41 general and can be used for fragility analysis whenever there is a need to have multiple
42 probability distributions to represent the uncertainty of the fragility variables.

43 The framework is illustrated through application to earthquake mortality data for four
44 structural types obtained from the 2005 Pakistan earthquake combined with information
45 from PAGER (Earle et al. 2009; Jaiswal et al. 2009; Wald et al. 2010). This data will be
46 used in the development of the simple exponential distribution first, and then for
47 Bernoulli-exponential and Bernoulli-gamma models to better represent the zero and
48 nonzero mortality rates. In these analyses the focus is to evaluate the uncertainties in the
49 posterior mortality marginal distributions that combine the PAGER information and the
50 observed data and to identify the reduction of epistemic uncertainty.

51 **MORTALITY RATE MODELLING**

52 Past observations following major earthquakes have shown that deaths and injuries
53 occur primarily in structures that have either partially or completely collapsed (e.g.
54 Ferreira, Olivera and Mota de Sá 2011; Shoaf et al. 2005; Petal 2011). Structures that
55 have minor to moderate damage but no collapse rarely cause deaths, the exception being

56 deaths caused by falling objects or debris. Thus, the mortality rate, X , is defined in the
57 equation (1) as the fraction of deaths of the total occupants in a building or a structure
58 that has collapsed.

$$X = \frac{\text{Total number of deaths}}{\text{Total number of occupants}} \quad (1)$$

59 Models and data on earthquake casualties are very limited and as a result mortality
60 rates are highly uncertain. To capture this variability, the mortality rate, X , is modeled in
61 this paper using parametric probability distribution. The form of the probability density
62 function of X , $f_{X|\theta}(x|\theta)$, is not known and there are several candidate functions
63 examined in this paper. The parameters of the mortality rate probability distribution are
64 typically obtained from limited data and the uncertainty on the parameters reflects the
65 epistemic uncertainty in the model. Consequently, they are modeled as random variables.

66 In order to combine various sources of data and reduce the uncertainty in the
67 mortality rate model, the Bayesian framework is utilized to estimate the parameters of the
68 mortality rate probability distribution by combining information from different data
69 sources. The general Bayesian formulation for information updating and its application
70 are described in the following sections.

71 **BAYESIAN UPDATING MODEL**

72 The Bayesian formulation for vulnerability functions presented in this paper focuses on
73 mortality rates, however, it is general and can be applied to any other vulnerability
74 function analysis. Bayes' rule provides the basis for combining various sources of
75 information and data and enables treating the uncertainties in the parameters of the parent
76 distribution of the random variable X . Equation (2) states Bayes' rule as follows:

$$f_{\theta|X}(\theta|x) = \frac{f_{X|\theta}(x|\theta)f_{\theta}(\theta)}{\int_{\theta} f_{X|\theta}(x|\theta)f_{\theta}(\theta) d\theta} \quad (2)$$

77 where $x = \{x_1, x_2, \dots, x_n\}$ is the set of n independent observations of the random variable
78 X that has the underlying probability distribution $f_{X|\theta}(x|\theta)$, $f_{\theta}(\theta)$ is the 'prior
79 distribution' of the parameter θ that represents prior knowledge about the parameter

80 before observing any data; $f_{\theta|x}(\theta|x)$ is the ‘posterior distribution’ of the parameter that
81 represents the knowledge about the parameter after observing data.

82 **PRIOR/POSTERIOR DISTRIBUTION DISTRIBUTIONS OF θ**

83 One of the main challenges of the Bayesian approach is to select appropriate distribution
84 for the parameter(s) θ and to estimate the distribution based on the information that is
85 available. The variability captured by the distribution $f_{\theta}(\theta)$ reflects the epistemic
86 uncertainty that, with sufficient data, can be reduced.

87 Computing the posterior distribution using equation (2) can be algebraically complex
88 and may not have a closed form solution. In special cases, the posterior distribution
89 belongs to the same family of probability distributions as the prior distribution for a
90 particular parent distribution (or likelihood function). This family of prior and posterior
91 distributions is said to be ‘conjugate’ to the corresponding likelihood function. In such a
92 case, the posterior distribution can be compactly represented by the hyper-parameters
93 updated from the prior using the new information. Hyper-parameters are parameters that
94 describe the prior distribution of θ . For mathematical convenience, we use conjugate
95 distributions to model the parameter distributions. In the next section, the exponential and
96 gamma distributions will be used to model mortality rates and we will apply the
97 conjugate distributions for their parameters. Subsequently, a novel approach for
98 combining Bernoulli-exponential and Bernoulli-gamma distribution prior-posterior
99 parameters will be presented. Further discussion on conjugate prior-posterior
100 distributions can be found in Raiffa and Schlaiffer (2000), Rice (1999), and Ang and Tang
101 (2007).

102 **MARGINAL DISTRIBUTION**

103 For the purposes of practical applications, it is desirable to develop one distribution that
104 combines the uncertainty in the random variable X described by the conditional
105 distribution $f_{X|\theta}(x|\theta)$ and the uncertainty in the parameters θ described by $f_{\theta}(\theta)$.
106 Integrating over the range of values of each of the parameters of the parent distribution of
107 X we the marginal distribution of X is given by equation (3).

$$f_X(x) = \int_{\theta} f_{X|\theta}(x|\theta)f_{\theta}(\theta) d\theta \quad (3)$$

108 Either the prior or the posterior distribution of θ can be used in equation (3) to obtain the
 109 marginal distribution of X . Equation (3) cannot be obtained in closed form and is
 110 typically estimated using numerical integration.

111 DEVELOPMENT OF BAYESIAN MODELS FOR MORTALITY RATES

112 SELECTION OF MORTALITY RATE DISTRIBUTION

113 In order to select appropriate distributions for mortality rates, analysis was performed
 114 first on existing mortality rates data and the general trends were observed. [Mortality rates](#)
 115 [are defined as number of deaths divided by the number of occupants](#). Data were obtained
 116 for the four categories of construction classes defined as Concrete, Stone, Mud and Stone,
 117 and All combined. The data from the 2005 Pakistan earthquake consists of number
 118 occupants and number of deaths for collapsed buildings in the affected area. [The Pakistan](#)
 119 [earthquake data were collected by household questionnaire surveys carried out in June](#)
 120 [2016 in collaboration with the University of Peshawar in the local language](#). [In all, 530](#)
 121 [surveys were done. The interviews assembled two different kinds of information,](#)
 122 [descriptive and factual. In many ways the descriptive accounts provide the best evidence](#)
 123 [of what occurred and what was observed by the survivor. There are some limitations to](#)
 124 [this data set as a representative sample of those affected. For example, we could only](#)
 125 [interview families who survived. For obvious reasons families with no survivors or those](#)
 126 [that had migrated could not be interviewed. This could mean there are more reports from](#)
 127 [people living in better building types, and from those on flatter lands in our data](#)
 128 [set. Returned forms for the uninjured were few for Pakistan. This could be due to the bias](#)
 129 [introduced with the selection of heavily damaged villages in Pakistan or to do with the](#)
 130 [responders and interviewers not understanding that information on the uninjured and their](#)
 131 [survival were just as important as those seriously injured. Mortality rates defined as](#)
 132 [number of deaths divided by the number of occupants were obtained for each structural](#)
 133 [type. The number of mortality rates number of data used for each construction type is](#)
 134 [listed in Table 1. The sample mean, standard deviation and coefficient of variation \(CoV\)](#)
 135 [for Mortality rates defined as number of deaths divided by the number of occupants were](#)
 136 [obtained for each structural type mortality rates in each building category are also listed in](#)
 137 [that table.](#)

138 **Table 1.** Sample Statistics for [Casualties-Mortality Rates](#) by Building Construction Class

Construction Class	Number of Samples	Sample Mean	Sample Std. Dev.	Sample CoV
Concrete	248	0.125	0.195	1.556
Stone	155	0.092	0.140	1.530
Mud and Stone	41	0.072	0.114	1.590
All	444	0.107	0.181	1.684

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140 Several distributions were tested and it was found that the exponential and the gamma
 141 parametric distributions fit the data well. Empirical cumulative distribution functions
 142 (eCDF) of the mortality rate data were developed from the given mortality rate data and
 143 were compared with the cumulative distributions (CDFs) of exponential and gamma
 144 distribution.

145 The equations of the probability density function for the exponential and gamma
 146 probability densities are given by equations (4) and (6), respectively. The mean values
 147 and standard deviations for each distribution are given in equation (5) and (7).

$$f(x|\lambda) = \lambda e^{-\lambda x} \quad (4)$$

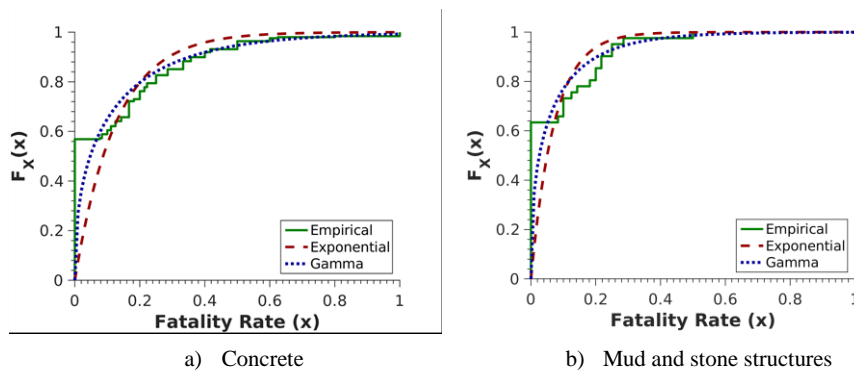
$$\mu = 1/\lambda \quad (5)$$

$$\sigma = 1/\lambda$$

$$f(x|\alpha, \beta) = \frac{\beta^\alpha}{\Gamma(\alpha)} x^{\alpha-1} e^{-\beta x} \quad (6)$$

$$\mu = \alpha/\beta \quad (7)$$

$$\sigma = \alpha/\sqrt{\beta}$$



148 **Figure 1.** Empirical CDF from fatality rate data and exponential and gamma distributions fitted
 149 fitted CDFs for (a) concrete structures (b) mud and stone structures.

150 Figures 1a and 1b show examples of eCDF's and fitted exponential and gamma
 151 distributions to the Pakistan 2005 data for concrete and stone structures. From that figure
 152 it can be seen that both the exponential and the gamma distributions follow the general

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153 pattern of the data, however, they underestimate the zero mortality rates. The same results
154 were observed with the remaining building categories in the data. In the next section, the
155 Bayesian updating only for the exponential distribution will be shown when using one
156 distribution for the entire range of mortality rate values. In the following sections, the
157 results for the combined Bernoulli and exponential and the Bernoulli and gamma
158 distributions will be presented as these capture the variations between zero and non-zero
159 mortality rates.

160 EXPONENTIAL BAYESIAN ANALYSIS

161 In the previous section, only the information from the observed data was used. Prior to
162 any data collection, information for Pakistan was available primarily from [the Prompt](#)
163 [Assessment of Global Earthquakes for Response \(PAGER\)](#), (Jaiswal et al. 2009). [The](#)
164 [United States Geological Survey \(USGS\) developed the PAGER framework to estimate](#)
165 [fatalities caused by earthquakes. In PAGER, fatality rates were estimated using a](#)
166 [combination of fatality statistics from previous earthquakes and expert judgment. These](#)
167 [rates were estimated for multiple construction materials and they represent global rates](#)
168 [since they were obtained from worldwide data \(Jaiswal et al., 2009\)](#). For the Bayesian
169 analysis, data from PAGER were used to estimate the prior distribution of the parameter
170 λ . The analysis is performed as follows.

171 The mortality rate X , ($0 \leq x \leq 1$) is characterized by the exponential distribution
172 given by equation (4) with parameter λ . The conjugate distribution on the parameter λ for
173 the exponential distribution is the gamma distribution given by equation (8).

$$f_{\Lambda}(\lambda|\omega, \varphi) = \frac{\varphi^{\omega}}{\Gamma(\omega)} \lambda^{\omega-1} e^{-\varphi\lambda} \quad (8)$$

174 where α and β are called the hyper-parameters of the probability distribution of λ . It
175 should be noted that these hyper-parameters are different from the ones that were used in
176 equation (6).

177 PRIOR DISTRIBUTION FOR λ

178 Prior mean values of the mortality rate are taken from the Proposed Fatality Rates for
179 implementation into PAGER. These are the fatality rate values given structural collapse

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180 provided in PAGER (Jaiswal et al. 2009). The coefficient of variation, CoV, is assumed
 181 to ~~be have a value of 0.30 and is kept~~ constant for all construction types, ~~with a value of~~
 182 ~~0.30~~. The fatality rates are presented as a ratio of the total number of occupants in
 183 completely collapsed buildings. The mean values for each structural type are given as
 184 follows:

- 185 • Concrete: 0.15
- 186 • Stone: 0.06
- 187 • Mud and stone: 0.06
- 188 • All: 0.11 (Evaluated by taking the weighted mean of concrete, stone, and mud and
 189 stone fatality rates where the weights are the number of structures in each group
 190 corresponding to which are 248, 155 and 41, respectively).

191 These values are also listed in Table 2 for completeness. The coefficient of variation
 192 (CoV) is assumed to be 0.3 for all the four construction types. Using these values for the
 193 mean and coefficient of variation, the hyper-parameters for the gamma distribution of the
 194 parameter λ are estimated and are listed in Table 2.

195 **Table 2.** Prior and posterior hyper-parameters for the gamma distribution on the parameter λ
 196 considering exponential-gamma conjugate pairs for different structural types.

Construction Class	ω_{prior}	φ_{prior}	Prior		$\omega_{posterior}$	$\varphi_{posterior}$	Posterior	
			Mean λ	CoV λ			Mean λ	CoV λ
Concrete	11.11	1.667	6.67	0.30	259.11	32.78	7.90	0.06
Stone	11.11	0.667	16.67	0.30	166.11	14.87	11.17	0.08
Mud and stone	11.11	0.667	16.67	0.30	52.11	3.62	14.39	0.14
All	11.11	1.222	9.07	0.30	285.11	30.65	9.30	0.59

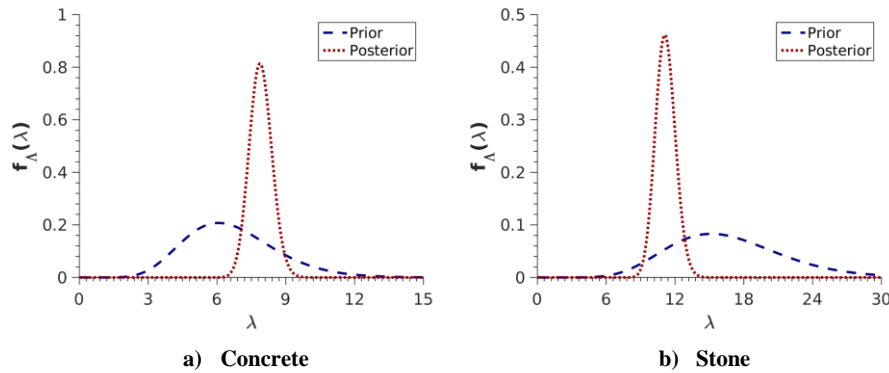
197 POSTERIOR DISTRIBUTION FOR λ

198 Since the gamma distribution is the conjugate distribution of the exponential probability
 199 density, the likelihood function does not need to be developed explicitly. The posterior
 200 distribution follows the same gamma distribution form as the prior, but with the posterior
 201 values of the hyper-parameters substituted for the prior ones. The hyper-parameters ω
 202 and φ for the posterior distribution on the parameter λ can be obtained using the
 203 following equation (see Ang and Tang, 2007):

$$\omega_{posterior} = \omega_{prior} + n \quad (9)$$

$$\varphi_{posterior} = \varphi_{prior} + \sum_{i=1}^n x_i$$

204 where x_i 's are the observed mortality rates from the data and n is the number of
 205 observations. Table 1 listed the number of observations from the 2005 Pakistan
 206 earthquake as well as the sample mean and standard deviation for each building type. The
 207 posterior hyper-parameters are listed in Table 2.



208 **Figure 2.** Prior and posterior gamma distributions of the exponential distribution parameter λ for
 209 (a) concrete structures and (b) stone structures.

210 Figure shows the prior and posterior distribution on the parameter λ for concrete and
 211 stone building types. The mean in each case has moved closer to the sample mean, and in
 212 all cases the standard deviation for the posterior is smaller than the prior showing that the
 213 epistemic error in the estimates has been reduced using this approach.

214 MARGINAL DISTRIBUTION ON MORTALITY RATES, X

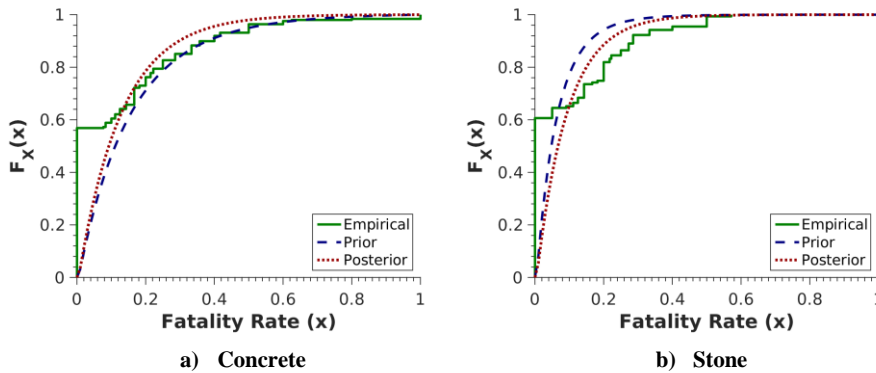
215 Marginal probability density function of mortality rate was defined by equation (3).
 216 Equation (3) was evaluated using numerical integration with increments of 10^{-4} for λ and
 217 10^{-2} for x . After computing the prior and posterior marginal distributions, the prior and
 218 posterior mean and standard deviation on mortality rates X are computed also using
 219 numerical integration. The results from these analyses for each of the structural types are
 220 given in Table 3. From these estimates, it is observed that the mean from the posterior
 221 marginal distribution is closer to the sample mean given in Table 1. The standard

222 deviation from the posterior marginal distribution is smaller than that the standard
 223 deviation from both the prior marginal distribution and the sample, which indicates that
 224 combining the heuristic information with the data reduced the overall uncertainty of
 225 mortality rate.

226 **Table 3.** Marginal prior, sample, and marginal posterior mean and coefficient of variation of
 227 mortality rates considering exponential-gamma conjugate pairs for different structural types.

Construction Class	Prior Marginal Mean, μ_x	Prior Marginal CoV, σ_x/μ_x	Posterior Marginal Mean, μ_x	Posterior Marginal CoV, σ_x/μ_x	Sample Mean	Sample CoV
Concrete	0.159	1.038	0.127	1.016	0.125	1.556
Stone	0.066	1.144	0.090	1.036	0.092	1.530
Mud and Stone	0.066	1.144	0.071	1.059	0.072	1.590
All	0.119	1.089	0.108	1.025	0.107	1.684

228
 229 Figure 3 shows the prior and posterior cumulative distribution functions (CDF) for
 230 concrete and stone building types. It can be observed that the posteriors functions fit
 231 the data well for values higher than zero. The zero mortality rate is not predicted well
 232 by either the prior or the posterior marginal distributions. A different approach will be
 233 considered in subsequent sections to capture this difference.



234 **Figure 3.** Prior and posterior marginal cumulative densities for exponentially distributed
 235 mortality rate for (a) concrete structures and (b) stone structures

236 **BERNOULLI-EXPONENTIAL BAYESIAN MODEL OF MORTALITY RATES**

237 In this section, zero mortality rates have been considered separately and Bernoulli
 238 Bayesian analysis performed on zero mortality rates is presented. Non-zero mortality
 239 rates are modeled again using exponential Bayesian analysis.

240 The mortality rate X , defined over the range ($0 \leq x \leq 1$) is now defined over two
 241 ranges. For that purpose, we use a Bernoulli distribution to describe the occurrence of a
 242 mortality rate equal to 0, p_0 , and we use the exponential probability to model the PDF of
 243 the mortality rate given that it is greater than 0. Therefore, the probability distribution of
 244 X is defined in equation (10).

$$f(x|\lambda, p_0) = \begin{cases} p_0 & \text{for } x = 0 \\ (1 - p_0)\lambda e^{-\lambda x} & \text{for } 0 < x \leq 1 \end{cases} \quad (10)$$

245 **Prior and Posterior Distributions for p_0 and λ**

246 A beta distribution was used to model the prior distribution of p_0 since it is the conjugate
 247 of a Bernoulli distribution and is given by equation (11).

$$f(p_0|a, b) = \frac{\Gamma(a + b)}{\Gamma(a)\Gamma(b)} p_0^{a-1} (1 - p_0)^{b-1} \text{ for } 0 < p_0 < 1 \quad (11)$$

248

249 where a and b are the hyper-parameters of the beta probability distribution of p_0 . Since
 250 the beta distribution is the conjugate of the Bernoulli density function, the posterior
 251 distribution on the parameter p_0 will also be a beta with posterior hyper-parameters
 252 parameters computed using the following equations (see Ang and Tang, 2007):

$$\begin{aligned} a_{\text{posterior}} &= a_{\text{prior}} + \sum_{i=1}^n 1\{x_i = 0\} \\ b_{\text{posterior}} &= b_{\text{prior}} + n - \sum_{i=1}^n 1\{x_i = 0\} \end{aligned} \quad (12)$$

253 where n is the total number of data points and $1\{x_i = 0\}$ takes the value of 1 when $x_i =$
 254 0 and 0 otherwise. The prior and posterior distributions of λ are again gamma as
 255 described previously. The prior Bernoulli-exponential distribution was set by using
 256 PAGER information. The values of the hyper-parameters for the gamma conjugate
 257 probability density of the exponential parameter λ were chosen randomly, and the prior
 258 mean value of p_0 , μ_{p_0} , was chosen so that the mean value of the prior distribution of X for
 259 all values greater than or equal to zero, given in Equation (3), approaches to the mortality
 260 rates reported by PAGER. The coefficient of variation CoV of p_0 is assumed to be 0.3 for
 261 all the four construction types. It was found that the results do not vary significantly with

262 random selection of the hyper-parameters. For the particular case of the Pakistan
 263 earthquake data, the posterior is governed by the data. Table 4 lists the sample statistics
 264 for the zero fatality observations for each of the structural types considered in the study.

265 The prior and posterior distributions of the parameter p_0 are shown in Figure 4. The prior
 266 and posterior parameters and the respective means and standard deviations are listed in
 267 Table 5. The prior and posterior hyper-parameter values for the gamma conjugate
 268 probability density of the exponential parameter λ are listed in Table 6. The
 269 corresponding probability densities for concrete and stone building types are shown in
 270 Figure 5. Table 6 provides posterior mean and standard deviations for the exponential
 271 distribution for each of the four structural classes and non-zero mortality rates. From
 272 Table 4, 5 and 6, it can be observed that the posterior mean values in all cases are
 273 considerably closer to the sample means. The standard deviations for the posterior
 274 distribution of p_0 and λ are again smaller than the prior values. These show that the
 275 incorporation of new data reduces the initial epistemic uncertainties.

276 **Table 4.** Prior and posterior parameters for the zero mortality rate parameter p_0 for different
 277 structural types

Construction Class	Number of samples	Houses with zero fatalities	Fraction with zero fatalities
Concrete	248	141	0.569
Stone	155	94	0.606
Mud and Stone	41	26	0.634
All	444	269	0.606

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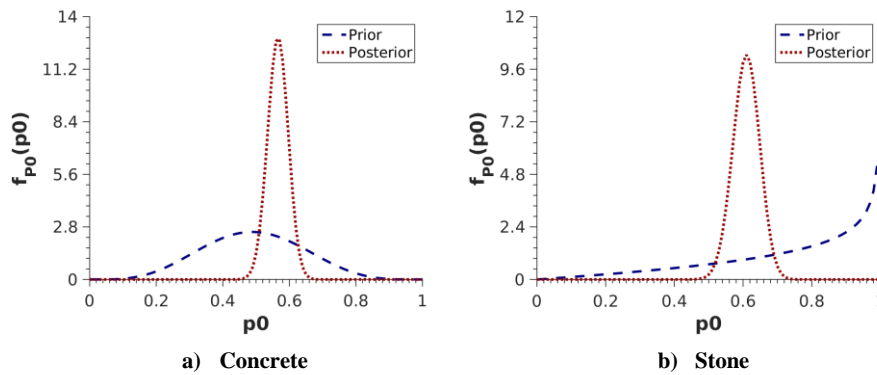
279 **Table 5.** Prior and posterior parameters for the zero mortality rate parameter p_0 for different
 280 structural types

Construction Class	a_{prior}	b_{prior}	Prior Mean p_0	Prior CoV p_0	$a_{posterior}$	$b_{posterior}$	Posterior Mean p_0	Posterior CoV p_0
Concrete	5.170	5.370	0.491	0.30	146.17	112.37	0.565	0.054
Stone	2.004	0.661	0.752	0.30	99.00	61.66	0.576	0.064
Mud and stone	1.948	0.627	0.757	0.30	27.95	15.63	0.577	0.112
All	3.793	2.484	0.604	0.30	169.79	110.48	0.606	0.048

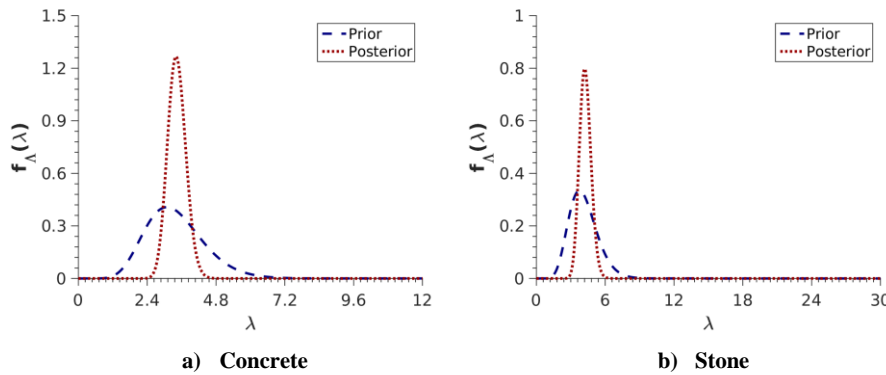
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282 **Table 6.** Prior and posterior parameters for the gamma distributed parameter λ considering
 283 exponential-gamma conjugate pairs for different structural types

Construction Class	ω_{prior}	φ_{prior}	Prior Mean λ	Prior CoV λ	$\omega_{posterior}$	$\varphi_{posterior}$	Posterior Mean λ	Posterior CoV λ
Concrete	11.11	3.27	3.40	0.30	118.11	34.38	3.44	0.09
Stone	11.11	2.69	4.13	0.30	72.11	16.89	4.27	0.12
Mud and stone	11.11	2.74	4.06	0.30	26.11	5.69	4.59	0.20
All	11.11	3.09	3.60	0.30	119.11	32.51	3.66	0.09



285 **Figure 4.** Prior and posterior beta distributions of p_0 for the Bernoulli distribution for zero
 286 fatalities for (a) concrete structures and (b) stone structures.



287 **Figure 5.** Prior and posterior gamma distributions of the exponential distribution parameter λ for
 288 (a) concrete structures and (b) stone structures.

289 **Marginal Distributions of Bernoulli-Exponential Mortality Rates**

290 Marginal probability density function of mortality rate is computed using the total
 291 probability theorem and is given in equation (13)

$$\begin{cases} \mu_{p_0} & \text{for } x = 0 \\ (1 - \mu_{p_0}) \int_{\lambda} f(x|\lambda)f(\lambda)d\lambda & \text{for } 0 < x \leq 1 \end{cases} \quad (13)$$

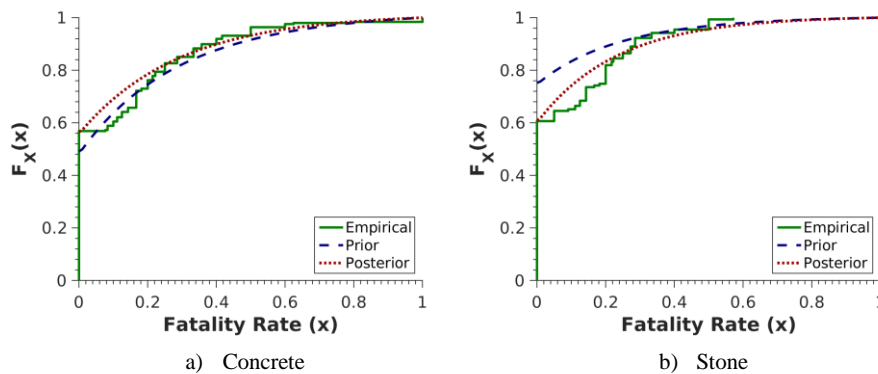
292 where $f(x|\lambda)$ is the probability distribution of the mortality rate X and $f(\lambda)$ is either the
 293 prior or the posterior of the probability density function of the parameter λ . μ_{p_0} is the
 294 mean value of p_0 obtained from the beta distribution of p_0 . The marginal distribution
 295 defined by Equation (13) was again evaluated using numerical integration.

296 Table 7 lists the marginal prior and posterior means and standard deviations for the
 297 mortality rates with Bernoulli-exponential distribution model. From these estimates it is
 298 observed that the mean from posterior marginal distribution is closer to the sample mean
 299 given in Table 1.

300 **Table 7.** Marginal prior and posterior means and coefficients of variation for the Bernoulli-
 301 exponential mortality model for different structural types.

Construction Class	Prior Marginal Mean, μ'_x	Prior Marginal CoV, σ'_x/μ'_x	Posterior Marginal Mean, μ''_x	Posterior Marginal CoV, σ''_x/μ''_x	Sample Mean	Sample CoV
Concrete	0.138	1.569	0.113	1.744	0.125	1.556
Stone	0.058	2.539	0.087	1.924	0.092	1.530
Mud and Stone	0.058	2.561	0.076	2.056	0.072	1.590
All	0.010	1.876	0.098	1.875	0.107	1.684

302



303 **Figure 6.** Prior and posterior marginal cumulative densities for the Bernoulli-exponentially
 304 distributed mortality rate for (a) concrete structures and (b) stone structures.

305 Figure 6 shows the marginal cumulative distribution functions (CDF) for the concrete
 306 and stone structural classes. It can be observed that in all the cases the posterior
 307 distributions fit the data closely for all values of mortality rate. More importantly, the
 308 distributions appear to reflect the zero mortality rate better than when only the
 309 exponential distribution was used to model X . Thus, modeling the zero and nonzero
 310 mortality rates separately can have a significant impact on the fitting of the Pakistan data.

311 **BERNOULLI-GAMMA BAYESIAN ANALYSIS**

312 From previous analysis, in almost all cases it was found that the gamma distribution fits
 313 the data better than the exponential distribution particularly for high values of mortality
 314 rates. Thus, a combined Bernoulli-gamma model is developed for the zero and non-zero
 315 mortality rates.

316 The occurrence of a mortality rate X equaling 0 is again defined as a Bernoulli
 317 distribution with probability p_0 , and the distribution of X given that it is greater than 0 is
 318 defined as a gamma distribution. Therefore, in this case the probability distribution of X
 319 is defined according to equation (14).

$$f(x|\alpha, \beta, p_0) = \begin{cases} p_0 & \text{for } x = 0 \\ (1 - p_0) \frac{\beta^\alpha}{\Gamma(\alpha)} x^{\alpha-1} e^{-\beta x} & \text{for } 0 < x \leq 1 \end{cases} \quad (14)$$

320
 321 The Bayesian analysis of the Bernoulli distribution remains the same as described in
 322 the previous section. The conjugate distribution of the gamma distribution for the non-
 323 zero mortality rates is given by equation (15). This conjugate distribution has
 324 $p, q, r,$ and s as hyper-parameters of the joint probability distribution of α and β . Then,
 325 the posterior distribution on the parameter will have the same form as equation (14) with
 326 the values of the hyper-parameters updated with the information obtained from the field
 327 observations. The relationship between the prior and the posterior hyper-parameters for
 328 the probability density are given by equation (16).

$$f(\alpha, \beta) = \frac{p^{\alpha-1} e^{-\beta q}}{K \Gamma(\alpha)^r \beta^{-\alpha s}} \quad \text{for } \alpha > 0, \beta > 0 \quad (15)$$

$$\begin{aligned}
K &= \int_0^{\infty} \frac{p^{\alpha-1} \Gamma(s\alpha + 1)}{\Gamma(\alpha) r q^{s\alpha+1}} \\
p_{\text{posterior}} &= p_{\text{prior}} P \\
q_{\text{posterior}} &= q_{\text{prior}} + S \\
r_{\text{posterior}} &= r_{\text{prior}} + n_{\text{non-zero}} \\
s_{\text{posterior}} &= s_{\text{prior}} + n_{\text{non-zero}} \\
P &= \prod_{\{i=1,2,\dots,n|x_i \neq 0\}} x_i \\
S &= \sum_{\{i=1,2,\dots,n|x_i \neq 0\}} x_i \\
n_{\text{non-zero}} &= \sum_{i=1}^n 1\{x_i \neq 0\}
\end{aligned} \tag{16}$$

329

330 **Prior and Posterior Distributions for p_0 and the Gamma Parameters α and β**

331 As before the prior mean values of mortality rate are taken from PAGER. The prior
332 values of parameters $p, q, r,$ and s are chosen randomly and different values were tested.
333 It was observed that the posterior distribution is not affected by this choice of prior values
334 as the data dominate the posterior parameters. Again, the prior mean value of $p_0, \mu_{p_0},$ was
335 chosen so that the mean value of the prior distribution of X for all values greater than or
336 equal to zero, given in Equation (3), approaches to the mortality rates reported by
337 PAGER, and the coefficient of variation of p_0 is assumed to be 0.3 for all the construction
338 types.

339 In this analysis, the prior, sample and posterior mean of the zero mortality rates were
340 taken identical to the values reported in Table 5 and are repeated here for completeness.
341 The prior and posterior hyper-parameters for the beta conjugate distribution of the
342 Bernoulli model are given in Table 8. Table shows the values of the prior, sample and
343 posterior means for the Bernoulli-gamma combined distributions for the four structural
344 types considered in this analysis.

345 **Table 8.** Prior and posterior hyper-parameters of the conjugate distribution of the gamma-
346 distributed non-zero mortality rates

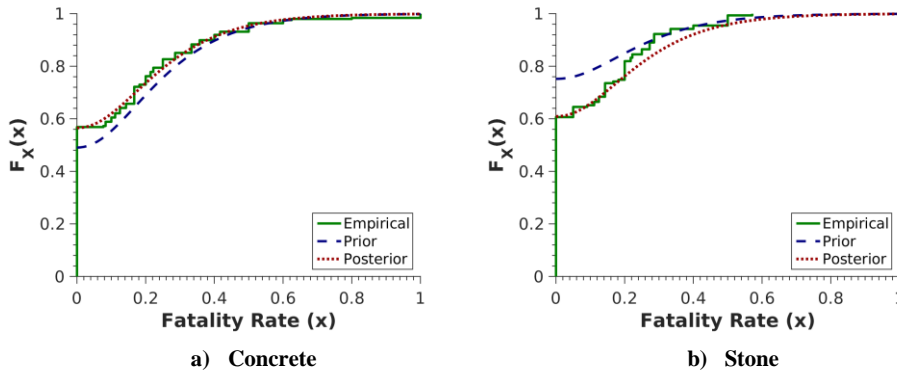
Construction Class	p_{prior}	q_{prior}	r_{prior}	s_{prior}	$p_{posterior}$	$q_{posterior}$	$r_{posterior}$	$s_{posterior}$
Concrete	2	1.23	1.50	1	1.43e-66	32.34	108.5	108
Stone	2	1.23	1.50	1	1.50e-43	15.43	62.5	62
Mud and stone	2	1.23	1.50	1	9.13e-12	4.18	16.5	16
All	2	1.23	1.50	1	3.18e-70	30.65	109.5	109

347 **Marginal Distributions of Bernoulli-Gamma Mortality Rates**

348 Marginal probability density function of non-zero mortality rate can be computed using
 349 the total probability theorem using equation (15).Th

$$f(x) = \begin{cases} \mu_{p_0} & \text{for } x = 0 \\ (1 - \mu_{p_0}) \iint f(x|\alpha, \beta) f(\alpha, \beta) d\alpha d\beta & \text{for } 0 < x \leq 1 \end{cases} \quad (17)$$

350
 351 where $f(x|\alpha, \beta)$ is the parent distribution of the mortality rate X and $f(\alpha, \beta)$ is the joint
 352 probability density function of the parameters α, β . μ_{p_0} is the mean value of p_0 obtained
 353 from the beta distribution of p_0 . The marginal distribution defined by equation (17) is
 354 again evaluated using numerical integration. Figure 7 shows the cumulative posterior
 355 marginal distribution function for all four structural classes as compared to the data. In all
 356 the cases the posterior distributions fit the data very closely for all values of mortality
 357 rate. This fit is significantly better than any of the previous combinations of analyses.



358 **Figure 7.** Posterior marginal cumulative densities for the Bernoulli-Gamma distributed mortality
 359 rate for (a) concrete structures (b) stone structures (c) mud and stone structures and (d) all
 360 structures

361

362 **Table 9.** Marginal prior and posterior means and standard deviations for the Bernoulli-Gamma
363 distributed mortality rate model for different structural types

Construction Class	Prior Marginal Mean, μ'_x	Prior Marginal CoV, σ'_x/μ'_x	Posterior Marginal Mean, μ_x	Posterior Marginal CoV, σ_x/μ_x	Sample Mean	Sample CoV
Concrete	0.150	1.292	0.1278	1.460	0.125	1.556
Stone	0.060	2.163	0.1026	1.436	0.092	1.530
Mud and Stone	0.060	2.281	0.1043	1.424	0.072	1.590
All	0.110	1.566	0.1145	1.475	0.107	1.684

364

365 Table 11 shows the marginal posterior mean and standard deviation for the various
366 structural types considered in the study. The mean values of the marginal distributions are
367 very close to the mean values obtained from the posterior Bernoulli-gamma distribution.
368 The standard deviation of the marginal mortality rate is slightly lower than the standard
369 deviations obtained from the posterior mortality rate analysis before integrating over the
370 uncertainties on the parameters.

371

CONCLUSIONS

372 In this paper a Bayesian formulation is presented for developing vulnerability functions
373 and the methodology is used for treating the uncertainties in earthquake mortality rate
374 data. Three different models are presented and tested with information from PAGER and
375 from the 2005 Pakistan earthquake. The models included exponentially distributed
376 mortality rates for all values greater than or equal to zero, a combined Bernoulli-
377 exponential model and a combined Bernoulli-gamma model for zero and non-zero
378 mortality rates. The Bayesian formulation for the exponential distribution with gamma-
379 distributed hyper-parameters is first presented. Values for hyper-parameters of the prior
380 distributions are developed using the mortality rates provided in PAGER and by
381 assuming that the coefficient of variation is fixed at 0.3. The posterior hyper-parameters
382 are obtained by combining the prior and data from Pakistan. In addition, the Bayesian
383 marginal prior and posterior probability densities and cumulative distributions are
384 computed through numerical integration.

385 Based on the analysis of the exponential model, it is found that the zero mortality
386 rates are not well represented and introduce a bias on the mortality rates greater than zero
387 prompting a separate treatment of the zero and non-zero mortality rates. The Bernoulli
388 distribution is used for the zero mortality rate and either an exponential or gamma
389 distribution is used for the non-zero mortality rate referred to respectively as the
390 Bernoulli-exponential and the Bernoulli-gamma models. Novel Bayesian formulations
391 are introduced for the Bernoulli-exponential and the Bernoulli-gamma models. The
392 conjugate distribution for the Bernoulli distribution parameter is the beta. The
393 exponential model remains the same as in the first analysis. A conjugate distribution for
394 the gamma non-zero rates is then defined and used for the Bayesian analysis of the
395 Bernoulli-gamma model. The formulations for the Bayesian marginal distributions that
396 integrate over all the parameter pdf's are developed for all models. These distributions
397 are evaluated numerically as closed form solutions cannot be obtained. Prior and
398 posterior mean values, standard deviations and coefficients of variation are also estimated
399 for all models.

400 Based on the analysis conducted for the Bernoulli-exponential and the Bernoulli-
401 gamma combined models, it is found that the Bernoulli-gamma functions are closest to
402 the observed data. In majority of cases, both the Bernoulli-exponential and the Bernoulli-
403 gamma models have posterior CoV's that are considerably smaller than those for the
404 prior or data pointing to one of the main advantages of using Bayesian analysis. For the
405 Bernoulli-gamma model, the posterior marginal CoV's of the casualty rates are smaller
406 than the prior CoV's, except for in one case. It is recommended that the Bernoulli-gamma
407 model be used as this model appears to best capture the zero and the non-zero rates.

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411

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